

## STRUCTURE OF NON-WOVEN FABRICS

Part III: The Relationship Between The Number of Fibres Drawn  
By The Needle And The Magnitude of Penetration.

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ABSTRACT

Although there are many investigations about mechanically bounded non-woven fabrics, but most of the results published in these investigations are explained qualitatively [1-3] rather than quantitatively. This could be partially due to lack of any mathematical models in this field. This work is considered to be an attempt to establish a mathematical model that could relate the number of fibres around the needle barbs within penetration depth ( $x$ ), with the maximum number of fibres drawn by the needle and the differential number of fibres in the batt in depth ranging between ( $x$ ) and ( $x + dx$ ).

Such model would be enable the estimation of the effect of each of these factors separately and could also be used to predict the stitching efficiency and stitching index.

Key-Words:-

- $N_x$  = number of fibres around the needle barbs in length ( $x$ ),
- $N_p$  = maximum number of fibres drawn by the needle,
- $dN_x$  = differential number of fibres in the batt in depth ranging between ( $x$ ) and ( $x + dx$ ),
- $dN_t$  = number of fibres missed (or left) by the needle during the needle upper-stroke,
- $N_d$  = needling density (needle/m<sup>2</sup>),
- $I$  = needling index,
- $t$  = thickness of batt (mm),
- $K_1$  = down-stroke constant and
- $K_2$  = up-stroke constant.

1. INTRODUCTION

Non-woven is comparatively a new technology to produce textile fabrics. The basic idea of this technology is to produce a fabric direct from fibres.

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Non-wovens can principally be manufactured by three major methods namely:-

- 1- Mechanical bonding; using needle felting machines,
- 2- Chemical bonding, using binders,
- 3- Thermal bonding, using thermoplastic fibres or fibres with lower melting temperature.

To produce NW. fabrics direct from fibres the following processing steps are absolutely necessary:

- 1- Fibre opening and blending - these processes are the same or similar as in every spinning mill,
- 2- Fibre carding on woollen cards - generally high - production carding machines are necessary,
- 3- Cross - lapping; the carded web - with this process the area weight and the laying width are determined,
- 4- Mechanical bonding with the help of needle felting machines (needle loom) and
- 5- Finishing process.

#### 1.1. Needling Process

Figure (1) illustrate schematically the constructive features of downstroke needle loom and the action of felting needles. The felting needles catch some of the fibres during their downward movement through the fibre batt and transport them through the holes of the stitching plate. The whole fibre structure becomes in this way active and a considerable number of fibres is displaced from their horizontal position towards vertical position.

The fibres are feed at the moment when the needles start their upstroke movement. Many fibres jump back due to the crimp and elasticity, many are broken and many slip just through the barbs. Some fibres protrude out of the stitching plate and their tails are flattened during the forward movement (advance) of the felt. At the same time needles once again start their downstroke movement and bring other fibres with them. There is the possibility that many get bound (interlaced or entangled) during this continuous fibre transport.

#### 2. THE THEORITICAL NEEDLING

Suppose the following:-

No. of fibres around the needle barbs in length  $(x) = N_x$ ,  
Maximum number of fibres drawn by the needle =  $N_p$ ,  
Differential number of fibres drawn by barbs in  $P$  depth ranging between  $x$  and  $x + dx = dN_x$ .

$$\begin{aligned}
 dN_n &= Q_1 \left( \frac{N_p - N_x}{N_p} \right) \cdot dx \\
 &= Q_1 \left( 1 - \frac{N_x}{N_p} \right) \cdot dx
 \end{aligned} \quad (1)$$

Suppose the number of fibres missed (or left) by the needle during the needle upper-stroke is  $dN_z$

$$dN_z = Q_2 \left( \frac{N_x}{N_p} \right) \cdot dx \quad (2)$$

from equs. (1 and 2) the number of reinforcing fibres in a distance  $dx$  is:

$$\begin{aligned}
 dN_x &= dN_n - dN_z \\
 &= Q_1 \left( 1 - \frac{N_x}{N_p} \right) dx - Q_2 \frac{N_x}{N_p} \cdot dx \\
 &= \left[ Q_1 - N_x \left( \frac{Q_1}{N_p} + \frac{Q_2}{N_p} \right) \right] dx \\
 &= \left[ Q_1 - \frac{N_x}{N_p} (Q_1 + Q_2) \right] dx
 \end{aligned} \quad (3)$$

by integrating equ. (3)

$$\begin{aligned}
 \int dN_x &= \int \left[ Q_1 - \frac{N_x}{N_p} (Q_1 + Q_2) \right] dx \\
 &= \int \frac{dN_x}{Q_1 - \frac{N_x}{N_p} (Q_1 + Q_2)} = \int dx \\
 x+C &= -\frac{1}{\frac{Q_1 + Q_2}{N_p}} \ln \left| Q_1 - (Q_1 + Q_2) \frac{N_x}{N_p} \right|
 \end{aligned} \quad (4)$$

But from the initial conditions:-

$$\begin{aligned}
 N_x &= 0 \text{ at } x = 0 \\
 C &= -\frac{N_p}{Q_1 + Q_2} \ln \left| Q_1 \right|
 \end{aligned} \quad (5)$$

Subs. in equ. (4)

$$\begin{aligned}
 x &= -\frac{N_p}{Q_1 + Q_2} \left[ \ln \left| Q_1 - \frac{Q_1 + Q_2}{N_p} N_x \right| - \ln \left| Q_1 \right| \right] \\
 &= -\frac{N_p}{Q_1 + Q_2} \cdot \ln \left| 1 - \frac{Q_1 + Q_2}{Q_1} \cdot \frac{N_x}{N_p} \right| \\
 &= -x \frac{Q_1 + Q_2}{N_p} = \ln \left| 1 - \frac{Q_1 + Q_2}{Q_1} \cdot \frac{N_x}{N_p} \right| \\
 e^{-x \frac{Q_1 + Q_2}{N_p}} &= 1 - \frac{Q_1 + Q_2}{Q_1} \cdot \frac{N_x}{N_p} \\
 N_x &= \frac{Q_1 N_p}{Q_1 + Q_2} \left[ 1 - e^{-x \frac{Q_1 + Q_2}{N_p}} \right] \quad (6)
 \end{aligned}$$

at  $x = 0$ ,  $N_x = 0$ , which means that the needle has not penetrated yet the ball of fibres, and when  $x \rightarrow \infty$ , then

$$N_x = \frac{Q_1}{Q_1 + Q_2} \cdot N_p \quad (7)$$

But actually this does not occur, and the number of fibres pushed by the needle will be less than that of equ. (7), but more than that of equ. (6). From equ. (7), the ratio  $N_x/N_p$  could be used to indicate the efficiency of needling, and the

ratio  $\frac{Q_1}{Q_1 + Q_2}$  will represent the same thing.

Subst. from equ. (6) in equ. (2)

$$\begin{aligned}
 dN_z &= Q_2 \cdot \frac{N_x}{N_p} \cdot dx \\
 &= \frac{Q_1 Q_2}{Q_1 + Q_2} \left[ 1 - e^{-x \frac{Q_1 + Q_2}{N_p}} \right] dx \quad (8)
 \end{aligned}$$

$$\text{and } \frac{dN_z}{dx} = \frac{Q_1 Q_2}{Q_1 + Q_2} \left[ 1 - e^{-x \frac{Q_1 + Q_2}{N_p}} \right] \quad (9)$$

where  $x$  = displacement of the needle,

$$\text{if } q_1 = \frac{Q_1}{N_p} \text{ and } q_2 = \frac{Q_2}{N_p}$$

$$\text{then, } \frac{dN_z}{dx} = N_p \frac{q_1 q_2}{q_1 + q_2} \left[ 1 - e^{-x (q_1 + q_2)} \right] \quad (10)$$

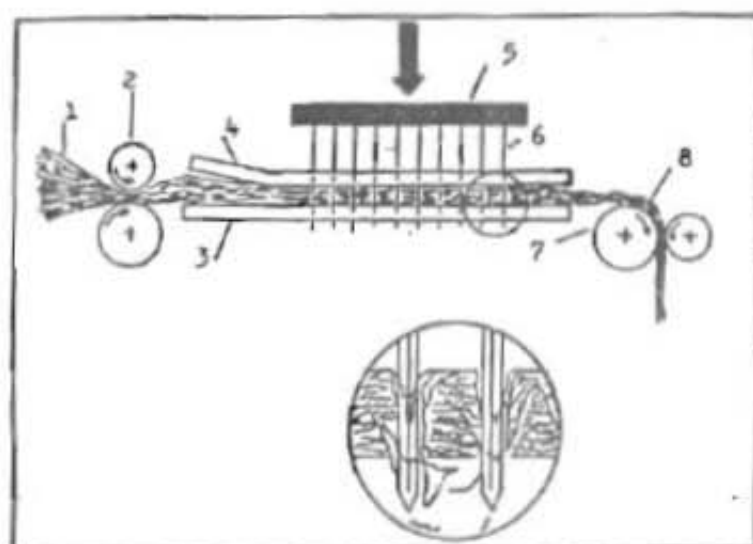


Fig.(1) Basic principles of needle felting technology.

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|-----------------------|-------------------|
| 1- fibre batt         | 2- feeding roller |
| 3- bottom plate       | 4- stripper plate |
| 5- needles board      | 6- felting needle |
| 7- drawing-off roller | 8- needle felt.   |

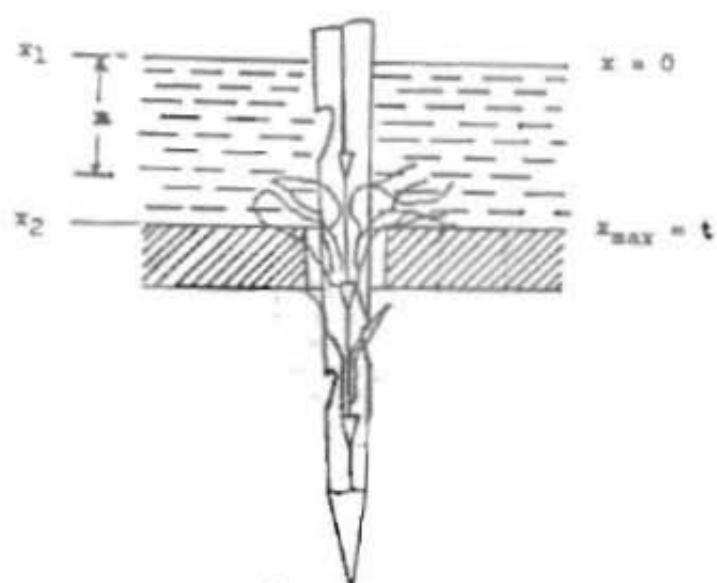


Fig.(2) Needle penetration through the batt.